

Buckling Restrained Braced Frames

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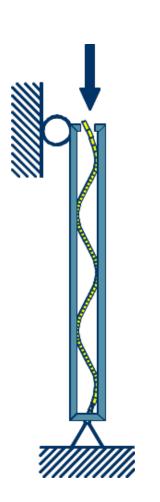
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Buckling Restrained Braced Frames

- Background
- Introduction to US practice
- Use today
- Ongoing issues



- Concept in India
 - Sleeved column
 - Decoupled stress and flexural buckling
 - Minimum-weight compression member
 - Energy absorption in compression (later)







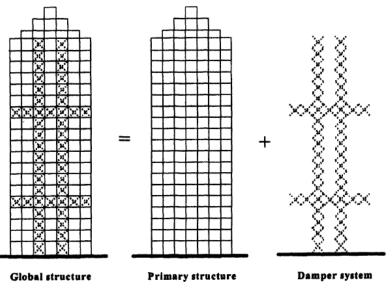
Use in Japan

1970s

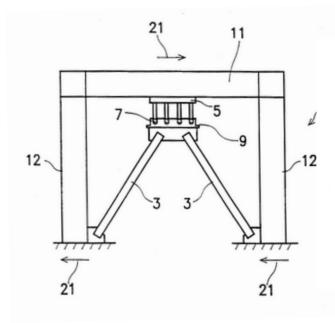
Developmental research on unbonded braces

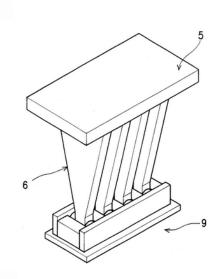
- 1980s
 - Use as hysteretic damping device

Similar to ADAS devices

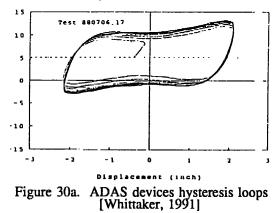








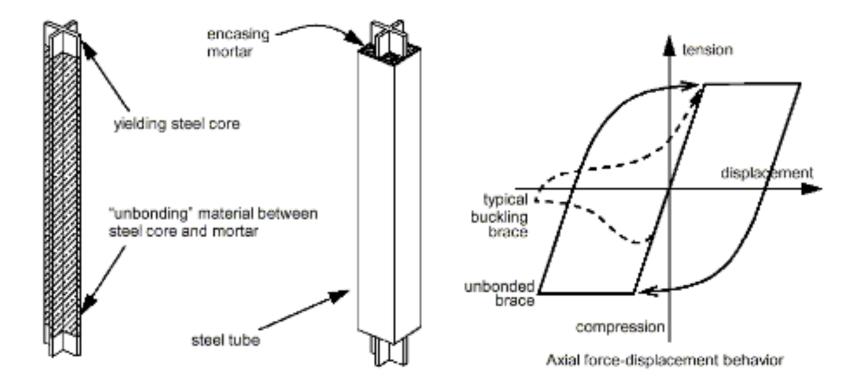
Shear Force (kips)



ADAS



Whittaker



Unbonded brace



Nippon Steel

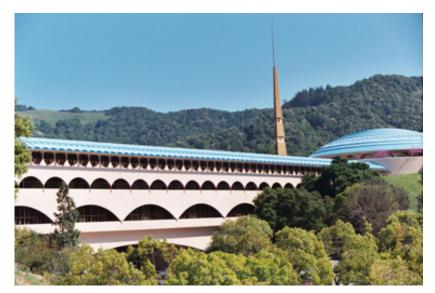
- First applications
 - New construction
 - 1999: Plant & Environmental Sciences Building, UC Davis





ARUP

- First applications
 - Retrofit
 - 2000: Marin County Civic Center Hall of Justice
 - 2002: Wallace F. Bennett
 Federal Building, Salt Lake City





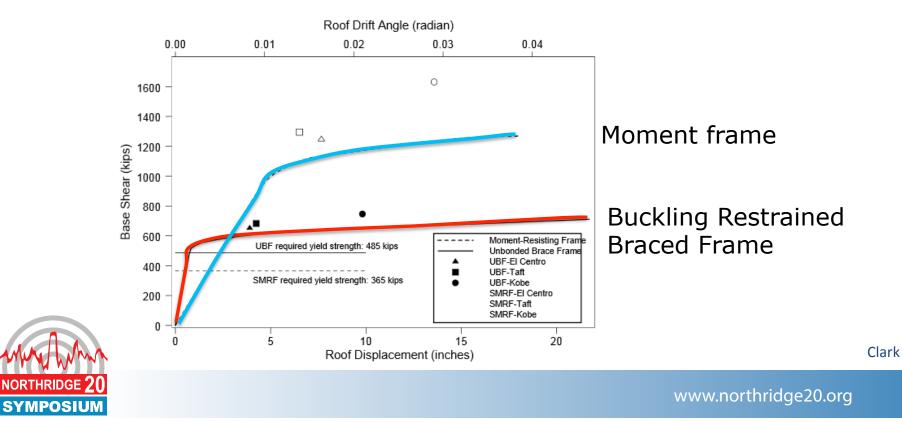
Crosby Group



Reaveley Engineering

US Design approach

- Primary lateral-load resisting system
 - Not as supplemental damping
- Controlled (limited) overstrength



Introduction to US practice US Design approach Decoupled strength and stiffness

An alternative design approach for sizing the unbonded braces could be to use smaller L'_{br} as long as the increase of ε_{br} is acceptable. Such an approach will produce a higher brace stiffness K_{br} and better drift control. This demonstrates how variations in L'_{br} can be investigated to control the stiffness of the unbonded brace independent of its strength. Similarly, steels of various yield strengths can be considered, giving designers the opportunity to modify the strength of a braced frame while keeping its stiffness constant.

- Fine print: as long as the strain is acceptable
 - (Often it is not!)
 - (Stiffness better achieved through more or larger braces)
- Design similar to Eccentrically Braced Frames



- Post-Northridge context
 - Less reliance on building code
 - Testing basis
 - Project-specific testing
 - Limited extrapolation
 - Focus on material issues
 - Large strains
 - Low-cycle fatigue
 - Skepticism of calculated drift
 - Minimum drift (rotation) requirements for moment frames



Code context

- Testing basis
- Design basis
 - 1997 UBC & 2000 IBC
 - "Design Basis Earthquake"
 - Life safety
 - Maximum Considered Earthquake"
 - Collapse prevention
 - Important buildings
 - 2003 IBC
 - Maximum Considered Earthquake
 - Collapse prevention
 - 2/3 MCE?
- NORTHRIDGE 20 SYMPOSIUM

Byproduct/artifact of process?

Code context

- Design basis
 - Hazard level and performance goal pairing not consistently understood
 - Translation of system performance goal into element performance requirement not clear
- Move to make Buckling Restrained Braced Frames an available codified system

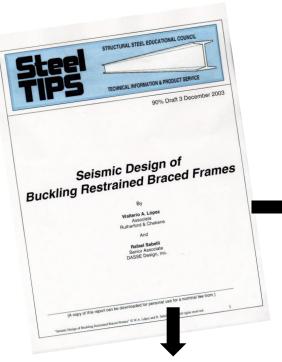


Code context

- SEAOC
 - Prominent role in UBC
 - Prominent role in SAC
 - Unclear role in ASCE 7/IBC
- SEAOC BRBF design provisions
 - Originated with SEAONC working group
 - Revised by AISC
 - Published 2003
 - Incorporated in to AISC Seismic 2005
 - AISC Seismic updated 2010



Steel Tips

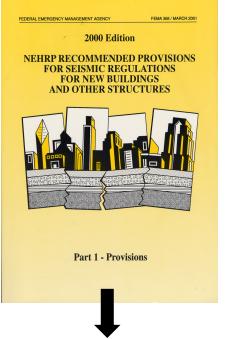


Design Guide to Aid

Designers and

Plan Reviewers

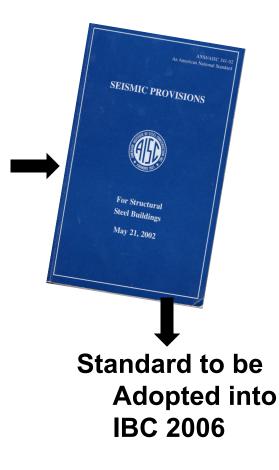
FEMA 450 (2003)



Guideline Includes

BRBF Provisions

AISC Seismic (2005)

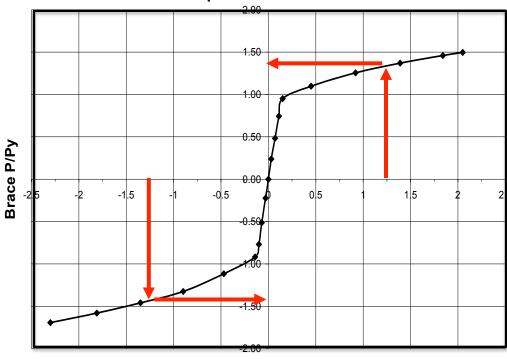


NORTHRIDGE 20 SYMPOSIUM

Code context

- 2003 BRBF design provisions
 - Strain-based overstrength
 - Amplified displacements used
 - $\blacksquare 1.5 \times C_d$
 - $R/C_d \sim 1.5$
 - Equivalent properties to Eccentrically Braced Frames
 - **R**
- Reasonable
- $\blacksquare \, \varOmega_o$
 - Reasonable; superseded for frame
- $\square C_d$
 - Too low, but consistent with other systems
 - Adjusted by 1.5 for strain and stroke





Sample BRB Backbone Curve

Brace Strain (%)



López and Sabelli

Code context

- 2003 BRBF design provisions
 - Testing required
 - Rotations
 - Limited extrapolation
 - "Similitude"
 - Maximum ductility
 - Cumulative ductility







Code context

2003 BRBF design provisions

- Minimum drift not considered for strain-hardening
 - Concentration of ductility not explicitly addressed for strain-hardening
 - Dependence on code-calculated drift
- Amplification based on limited study
 - Design Basis Earthquake



Code context

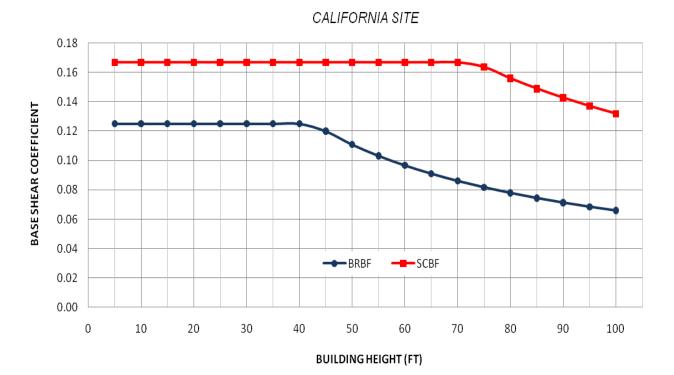
- 2005 BRBF design provisions
 - Amplified displacements used
 - 2 x *C_d*
 - MCE/DBE ~1.5
 - $R/C_d \sim 1.5$
 - 2% minimum drift considered for brace stroke
 - Strain-based overstrength
 - 2 × *C*_d
- 2010 BRBF design provisions
 - 2% minimum drift considered
 - Stroke
 - Strain hardening



- Codified system
 - One of the last systems not facing FEMA P-695
- Competing manufacturers
 - Competitive bid
 - Interchangeable products?
 - Strength/stiffness characteristics may be different
- Range of building types



LATERAL SYSTEM COMPARISON



Code provisions offer significant advantages for BRBF compared to other concentrically braced frames



CoreBrace

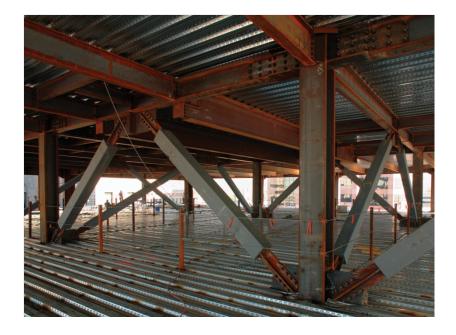
Low-rise concentrically braced frames

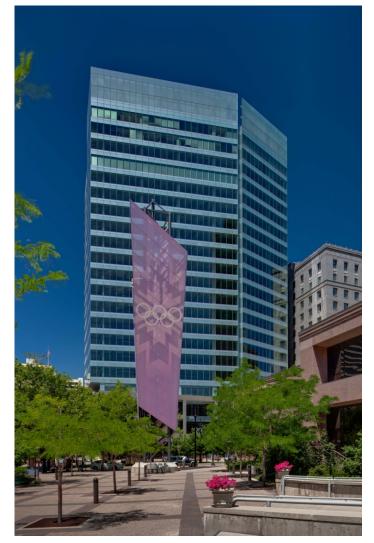




STAR Seismic

Use todayLarge buildings







CoreBrace

Use todayLarge buildings





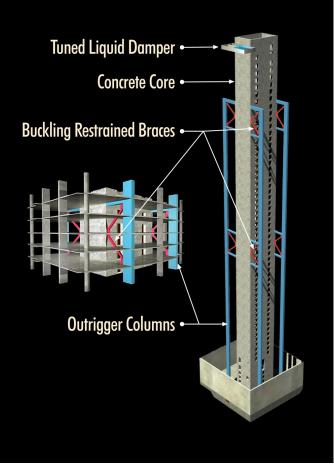


CoreBrace

Use todayForce-limiting applications



Outriggers





CoreBrace

Use todayForce-limiting applications



Outriggers

STAR Seismic



Use todayUnusual applications



Vertical brace in rocking frame



CoreBrace



Unusual applications

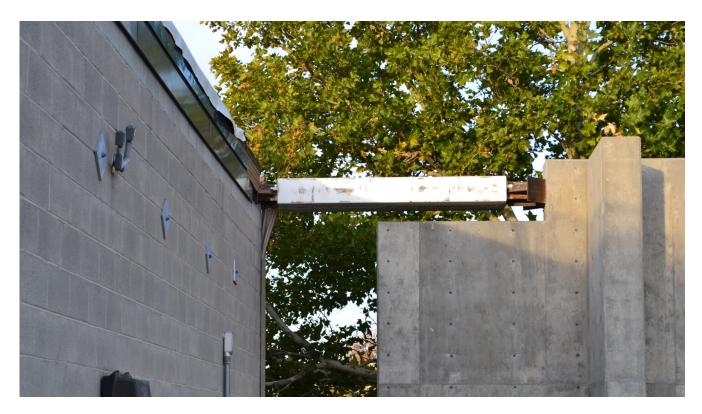




Dam structure

STAR Seismic

Unusual applications



Horizontal buttress

CoreBrace



Ongoing issues

Maximum Considered Earthquake

- Demands
 - Elongation
 - Maximum strain
- Performance
 - Collapse-prevention
 - Is ideal brace behavior necessary at MCE?
 - Appropriate reliability





Ongoing issues

Maximum Considered Earthquake

- Appropriate protocol
 - Strain-based overstrength
 - Current protocol may be too stringent
- Safeguard against under-prediction of strain
 - Short yield lengths
 - Result of (mentally) decoupling strength and stiffness
 - Minimum drift
 - Amplification of calculated maximum drift
- Utilization of existing test data



Thank you